

Precision test of the isotropy of light propagation

1 Introduction

Special relativity (SR) is a fundamental theory that describes how the concepts of space and time must be applied when describing physical phenomena in flat space-time. It therefore underlies all established theories of the forces of nature, from the gravitational and electromagnetic to the weak and strong nuclear forces. With the enormous advances in the technology of time, length, and frequency measurement, the effects of SR have become important even in daily measurement practice; for example, since 1983 the definition of the meter is based on the constancy of the velocity of light, one of the foundations of SR. Positioning by means of the global positioning system, a technique that is quickly penetrating modern life, can only be applied if the (special and general) relativistic frequency shifts of the atomic clocks onboard the satellites are taken into account. Because of its importance, SR has been and must be tested with increasing precision in order to provide a firm basis for its future application, be it within fundamental science or within measurement technology. Indeed, tests of SR and general relativity (GR) have a long and fascinating history that spans the whole period of modern physics, starting with the famous Michelson–Morley (MM) test of the isotropy of light propagation [1] that even predated the creation of SR (see Fig. 1). Over time, some of the tests have been improved in accuracy more than a million-fold, due to the application of new technologies as they came into operation, most notably atomic clocks and lasers.

Tests of relativity are also gaining more and more importance within the huge and challenging project of creating and verifying a theory that unifies all forces of nature. Such tests could, in the best case, discover a violation of some fundamental law that so far (i.e. at the current level of experimental accuracy) has been found to hold. In the ‘worst’ case, they will provide more and more stringent experimental bounds on the range of theoretical models of unification that theorists may conceive. In fact, many currently discussed models for a unified theory do violate the principles of special and general relativity. In string theory, for example, spontaneous symmetry breaking could cause Lorentz violation [2]. In loop gravity, modified Maxwell equations have been derived that are not necessarily Lorentz covariant [3, 4]. The natural energy scale for these theories is the Planck scale, $E_p \sim 10^{19}$ GeV. Direct experimentation at the Planck scale is, unfortunately, not feasible. It is, however, possible to search for residual effects with experiments operating at the attainable energies but featuring extremely high precision. This approach is also of great theo-

\[ \frac{\Delta c}{c} \leq 2 \times 10^{-19} \]

FIGURE 1 Accuracy of tests of the isotropy of electromagnetic wave propagation. $\Delta c = c(\theta) - c(\theta + \pi/2)$ is the established upper bound to the speed of light anisotropy. Experiments until 1930 were performed using optical interferometers, later experiments using electromagnetic cavities. The last three used lasers. The line is a guide for the eye.
ethical interest: even if a definitive version of quantum gravity is not found in the near future, it is possible to state the most general low-energy limit and test this 'effective' theory. Such a theory has recently been formulated as a Lorentz-violating standard model extension (SME) [5–7], which has also suggested new tests to be performed. High-precision tests can bound parameters of this theory and thus restrict the parameter space of a future theory of quantum gravity. Considering the current dearth of experimental guidance, even a tiny experimental hint for or against models of quantum gravity would be of considerable value for the process of formulation of the theory.

Here, we present an experiment that tests the isotropy of the speed of c (Michelson–Morley experiment) and improves the classic 1979 result of Brillet and Hall [8] by a factor of three. Moreover, it explicitly determines a set of bounds on seven parameters of the Maxwell sector of the SME, with an accuracy about two orders of magnitude higher than the pioneering measurement [9]. Other parameters of this theory have been determined in astrophysical observations. These, however, cannot access all parameters of this theory, whereas laboratory experiments can [6]. The most important results of the experiment have been reported in a letter [10]. Here, we describe in detail the theoretical background, technology, data analysis, and interpretation of the experiment and its results.

The basic concept of the MM experiment described in this work is to measure the difference \( \nu_x - \nu_y \) of the resonance frequencies \( \nu_x \) and \( \nu_y \) of two electromagnetic cavities pointing in orthogonal directions \( x \) and \( y \) in the laboratory frame as a function of the orientation and movement of the laboratory in space. The resonance frequencies of such a standing-wave Fabry–Pérot cavity are given by \( \nu_{x,y} = m c_{x,y}/(2L) \), where \( m \in \mathbb{N} \) is a constant mode number, \( L \) the cavity length, and \( c_{x,y} \) the phase velocities of light (actually the averages of the velocities for forward and backward propagation) along the axes of the cavities. The measured deviations of the cavity frequency difference from a constant are analyzed in terms of a possible Lorentz-violating variation of \( c \). In the framework of an assumed test theory (Sect. 2), bounds for parameters of the test theory can then be deduced. In practice, the frequency measurement is implemented by interrogating each cavity with a laser, and stabilizing ('locking') the laser frequency to the cavity (see Fig. 2). The frequencies of the lasers are then compared by measuring \( \nu_x - \nu_y \).

The experimental method we employ relies on optical resonators cooled to temperatures near absolute zero, called cryogenic optical resonators (COREs). The resonators (see Fig. 3), fabricated from ultra-pure crystalline sapphire, exhibit a very low thermal expansion coefficient at cryogenic temperature. Moreover, they exhibit a remarkable absence of creep, i.e. they show no intrinsic length changes due to material relaxation. Together, these features imply that the length of a CORE has an outstanding constancy. They are therefore very well suited for tests of the constancy of the speed of light of the optical wave inside the cavity, which are performed over long times.

We also note that experiments using electromagnetic cavities, especially cryogenic resonators, are now employed by other groups in ongoing and future high-precision tests of relativity. For example, Wolf et al. [11] reported a new Kennedy–Thorndike experiment (Sect. 2.2) using a cryogenic microwave resonator, which improves the limit previously set by our own test [12, 13]. A Michelson–Morley type of experiment using superconducting niobium microwave cavities, which was the first to report limits on the SME parameters as described above, was recently reported by Lipa et al. [9]. Space tests, to achieve the ultimate in performance in such experiments, with cavities on the International Space Station (SUMO [14]) and on a dedicated satellite (OPTIS [15]), are also being developed.

2 Theoretical framework

2.1 Standard model extension

Here we describe the SME and derive the hypothetical signal to be searched for in the experiment. The description of the SME is taken from [6] to introduce essential definitions required for the derivation.

The SME starts from a Lagrangian formulation of the standard model, adding all possible observer Lorentz scalars that can be formed from the known particles and Lorentz tensors. In the photonic sector, the Lagrangian is

\[ \mathcal{L} = -\frac{1}{4} F_{\mu\nu} \Lambda^\mu \Lambda^\nu + \frac{1}{2} (k_F) A^\mu A^\nu F_{\mu\nu} - \frac{1}{4} (k_F) A^\mu A^\nu F_{\mu\nu}, \]

where \( F_{\mu\nu} \) is the electromagnetic field tensor and \( A^\mu \) the vector potential. The first term is the usual Maxwell Lagrangian;
the other terms are Lorentz violating. The second term is expected to vanish for theoretical reasons and is constrained experimentally by cosmological birefringence measurements to levels well below those relevant here [16], so we can neglect it in what follows. The third term is proportional to a dimensionless tensor \((k_F)_{\mu\nu}\) that has the symmetries of the Riemann tensor plus a vanishing double trace. Thus, it contains 19 independent components.

The inhomogeneous Maxwell equations in vacuum following from this Lagrangian, namely

\[
\partial_\mu F^\mu_\nu + (k_F)_{\mu\alpha\beta\gamma} \partial^\alpha F^{\beta\gamma} = 0, \tag{2}
\]

and the homogeneous equations

\[
\partial_\mu \tilde{F}^{\mu\nu} = 0 \tag{3}
\]

can be written in analogy to the Maxwell equations in anisotropic media: with the \(3 \times 3\) matrices

\[
(k_{DE})^{jk} = -2(k_F)^{0jk}, \tag{4}
\]

\[
(k_{HH})^{jk} = \frac{1}{2} \epsilon^{kpq} \epsilon^{krs} (k_F)^{pqrs}, \tag{5}
\]

\[
(k_{DB})^{jk} = (k_F)^{0ipq} \epsilon^{kpq}, \tag{6}
\]

\[
(k_{HE})^{ij} = -(k_{DB})^{jk}. \tag{7}
\]

one can define \(D\) and \(H\) fields

\[
\begin{pmatrix} D \\ H \end{pmatrix} = \begin{pmatrix} 1 + k_{DE} & k_{DB} \\ k_{HE} & 1 + k_{HH} \end{pmatrix} \begin{pmatrix} E \\ B \end{pmatrix}, \tag{8}
\]

where \(I\) represents the \(3 \times 3\) unit matrix. The Maxwell equations can now be expressed as

\[
\nabla \times H - \partial_0 D = 0, \tag{9}
\]

\[
\nabla \times E + \partial_0 B = 0, \tag{10}
\]

\[
\nabla \cdot D = 0, \tag{11}
\]

\[
\nabla \cdot B = 0. \tag{12}
\]

Lorentz violation in electrodynamics thus corresponds to electrodynamics in anisotropic media. It is convenient to introduce the linear combinations

\[
(\tilde{\kappa}_{e^+})^{jk} = \frac{1}{2} (k_{DE} + k_{HB})^{jk}, \tag{13}
\]

\[
(\tilde{\kappa}_{e^0})^{jk} = \frac{1}{2} (k_{DB} + k_{HE})^{jk}, \tag{14}
\]

\[
(\tilde{\kappa}_{e^-})^{jk} = \frac{1}{2} (k_{DE} - k_{HB})^{jk} - \frac{1}{3} \delta^{jk} (k_{DE})^\nu_\nu, \tag{15}
\]

\[
(\tilde{\kappa}_{e^\nu})^{jk} = \frac{1}{2} (k_{DB} - k_{HE})^{jk}, \tag{16}
\]

\[
\tilde{\kappa}_\nu = \frac{1}{3} (k_{DE})^\nu_\nu. \tag{17}
\]

Two of these, \((\tilde{\kappa}_{e^+})^{jk}\) and \((\tilde{\kappa}_{e^0})^{jk}\), control the dependence of the propagation of light on its polarization and have been restricted by studying light from astronomical sources to < \(2 \times 10^{-32}\) [6], so we can assume \((\tilde{\kappa}_{e^+})^{jk} = (\tilde{\kappa}_{e^0})^{jk} = 0\) in the following. This restricts 10 of the 19 degrees of freedom of \((k_F)_{\nu\lambda\mu\nu}\). The further terms lead to a change \(\delta c\) of the phase velocity of light, which can be measured in cavity experiments like the one presented here.

The principle of such a measurement is studying the rotation invariance of the resonance frequency \(v_{cav}\) of an electromagnetic cavity, which is proportional to the velocity of light along the cavity axis. Thus, a Lorentz-violating shift \(\delta c / c\) of the velocity of light leads to an equal relative shift \(\delta v_{cav} / v_{cav}\) (assuming a constant cavity length \(L\), see below) independent of the polarization. It can be expressed within the SME as [6]

\[
\frac{\delta v_{cav}}{v_{cav}} = \frac{1}{2} \left[ (\tilde{N} \times \hat{E})^* (k_{HB})_{\text{lab}} (\tilde{N} \times \hat{E}) - \hat{E}^* (k_{DE})_{\text{lab}} \hat{E} \right]. \tag{18}
\]

Here, \(\tilde{N}\) denotes a unit vector that specifies the cavity orientation and \(\hat{E}\) a unit vector normal to \(\tilde{N}\) that specifies the polarization. The cavity frequency shift given by this expression is independent of the polarization if \(k_{DE} = -k_{HB}\) is inserted, which follows from \((\tilde{\kappa}_{e^+})^{jk} = 0\). The notation \((k_{HB})_{\text{lab}}, (k_{DE})_{\text{lab}}\) indicates that the matrices are given in the laboratory frame of the cavity.

The dependence of the cavity length on the elements of \((k_F)_{\nu\lambda\mu\nu}\) has been investigated in [17]: the Lorentz-violating electrodynamics necessarily leads to a modification of the Coulomb interaction given by \(k_{DE}\). Since the geometry of crystals is largely determined by Coulomb interactions, a change of the cavity length connected to \(k_{DE}\) will arise and modify the sensitivity of the relative frequency shift \(\delta v_{cav} / v_{cav} = \delta c / c - \delta L / L\) to Lorentz violation. For ionic materials, an increase of the sensitivity by material-dependent factors around 2 has been found [17]. For the material used for our COREs, sapphire (that has strong covalent bonds), the estimated increase is only a few percent [17]. We can therefore neglect the length change and proceed using (18).

### 2.1.1 Derivation of the signal in the laboratory frame

We use two frames of reference, in accordance with [6]: a Sun-centered standard frame (4-vector components in this frame are denoted by Greek indices, spatial components by capital Latin indices), and a laboratory frame (spatial components in the laboratory frame are denoted by small Latin indices \(a, b, c, \ldots\)).

The Sun-centered frame is suitable as a standard frame for expressing values of \((k_F)_{\nu\lambda\mu\nu}\) because it is inertial over all time scales relevant for the experiment. It has the \(X\) axis pointing towards the vernal equinox (spring point) at 0 h right ascension and 0° declination, the \(Z\) axis pointing towards the celestial north pole (90° declination), and the \(Y\) axis in the way needed to complete the right-handed orthogonal dreibein. Earth’s equatorial plane lies within the \(X–Y\) plane and the orbital plane of the Earth is tilted at an angle \(\eta \approx 23^\circ\) with respect to the latter. The time scale \(T\) is set by \(T_0 = 0\) when the Sun passes the spring point, which in 2001 happened on March 20, 13 h 31 min Universal Time (UT).

The laboratory frame has the \(x\) axis pointing south, the \(y\) axis east, and the \(z\) axis vertically upwards. The laboratory time scale is set by \(T_0\) at the instant when the \(y\) and the \(Y\) axes coincide, e.g. on March 20, 2001, 11:31 UT for our experiment, when in Konstanz the Sun passes the zenith. Then the direction of the radius of the Earth, drawn from the Earth’s
center to Konstanz and projected onto the equatorial plane, is parallel to the X axis, so that the y and the Y axes coincide.

To obtain the time dependence of the frequency of a cavity located on Earth from (18), the laboratory-frame matrices \((\kappa_{DE})_{\text{lab}}\) and \((\kappa_{HR})_{\text{lab}}\) can be obtained from the corresponding matrices in the Sun-centered standard frame using the transformations described in [6]. They involve Lorentz transformations according to the velocity \(\beta_{\oplus} \sim 10^{-4}\) of Earth’s orbit and the rotations from the Sun-centered frame to the laboratory defined by the rotation matrix

\[
R = \begin{pmatrix}
\cos \chi \cos \omega_{\oplus} T_{\oplus} & \cos \chi \sin \omega_{\oplus} T_{\oplus} & -\sin \chi \\
-\sin \omega_{\oplus} T_{\oplus} & \cos \omega_{\oplus} T_{\oplus} & 0 \\
\sin \chi \cos \omega_{\oplus} T_{\oplus} & \sin \chi \sin \omega_{\oplus} T_{\oplus} & \cos \chi
\end{pmatrix},
\]

where \(\chi \approx 42.3^\circ\) is the colatitude of Konstanz. The resulting time dependency of \(\delta \nu / \nu\) is given by the angular frequencies \(\omega_{\oplus} \approx 2\pi / (23\,\text{h}\,56\,\text{min})\) of Earth’s rotation and \(\Omega_{\oplus} = 2\pi / \text{yr}\). Due to the movement of the laboratory frame with \(\beta_{\oplus}\) and a velocity \(0 \leq \beta_{\oplus} \leq 1.5 \times 10^{-6}\) (dependent on the geographical latitude) due to Earth’s rotation, some suppressed by \(\beta_{\oplus}\) and/or \(\beta_{L}\).

The resulting frequency change of a single cavity can be expressed as [6]

\[
\frac{\delta \nu}{\nu} = A' + B' \sin 2\theta + C \cos 2\theta,
\]

where \(A', B', C\) and \(C_{0}, ..., C_{2}\) are combinations of components of \((\kappa_{F})_{\kappa_{0},\mu_{0}}\) defined in [6]. The primes are introduced to prevent confusion with \(A\) and \(B\) introduced later in (24). For our experiment, we measure the frequency difference \(\nu_{1} - \nu_{2}\) of a cavity oriented north–south and a cavity oriented east–west, so \(\theta_{1} = 0\) and \(\theta_{2} = 90^\circ\). Therefore,

\[
\frac{\delta (\nu_{1} - \nu_{2})}{\nu} = 2 C,
\]

where \(\nu \approx \nu_{1} \approx \nu_{2}\) is the average frequency. According to [6],

\[
C = C_{0} + C_{1} \sin \omega_{\oplus} T_{\oplus} + C_{2} \cos \omega_{\oplus} T_{\oplus} + C_{3} \sin 2\omega_{\oplus} T_{\oplus} + C_{4} \cos 2\omega_{\oplus} T_{\oplus}.
\]

The coefficients \(C_{0}, ..., C_{4}\) are given in Appendix E of [6]. We can simplify them by inserting \(\kappa_{\ominus} = \kappa_{\oplus} = 0\), the result of the astrophysical polarization measurements [5, 6]. \(C_{0}, ..., C_{4}\) are themselves time dependent, involving terms proportional to \(\cos \Omega_{\oplus} T\) and \(\sin \Omega_{\oplus} T\). For our experiment the difference of the time scales is \(\delta T = T - T_{\oplus} \approx 2\,\text{h}\). Substituting \(T = T_{0} + \delta T\) into the sine and cosine functions and using trigonometric relations, one obtains additional terms that are proportional to \(\sin \Omega_{\oplus} \delta T \approx 2 \times 10^{-3}\). We now substitute \(C_{0}, ..., C_{4}\) into (22).

The resulting signal can be written as a Fourier series with signal components at six different frequencies \(\omega_{0} = \omega_{\oplus}, \omega_{1} = \omega_{\oplus} \pm \Omega_{\oplus}, \omega_{2} = 2\omega_{\oplus}, \omega_{3} = \omega_{\oplus} \pm 2\Omega_{\oplus} = \omega_{\oplus} \pm \Omega_{\oplus} = \omega_{\oplus} \pm 2\Omega_{\oplus}:

\[
\frac{\delta \nu}{\nu} = C_{5} + s_{1} \sin \omega_{1} T_{\oplus} + s_{1} \cos \omega_{1} T_{\oplus} + s_{1} \sin \omega_{1} T_{\oplus}
\]

\[
+ c_{1} \cos \omega_{1} T_{\oplus} + s_{1} \sin \omega_{1} T_{\oplus} + s_{1} \cos \omega_{1} T_{\oplus}
\]

\[
+ s_{2} \sin \omega_{2} T_{\oplus} + c_{2} \cos \omega_{2} T_{\oplus} + c_{2} \sin \omega_{2} T_{\oplus}
\]

\[
+ c_{2} \cos \omega_{2} T_{\oplus} + s_{2} \sin \omega_{2} T_{\oplus} + c_{2} \cos \omega_{2} T_{\oplus}.
\]

The term \(C_{5}\) includes constants and terms that vary solely with the frequency \(\Omega_{\oplus}\). The remaining signal amplitudes are

\[
s_{1} = \frac{\beta_{\oplus}}{2} \sin \chi \cos \chi \sin [(\cos \eta + 1) (\tilde{k}_{\oplus})^{XY} - \cos \eta (\tilde{k}_{\oplus})^{XZ}],
\]

\[
c_{1} = \frac{\beta_{\oplus}}{2} \sin \chi \cos \chi \sin (\tilde{k}_{\oplus})^{YZ},
\]

\[
s_{1} = - \sin \chi \cos (\tilde{k}_{\ominus})^{YZ},
\]

\[
c_{1} = - \sin \chi \cos (\tilde{k}_{\ominus})^{XZ},
\]

\[
s_{1} = \frac{\beta_{\oplus}}{2} \sin \chi \cos \chi \sin [(\cos \eta - 1) (\tilde{k}_{\oplus})^{XY} - \sin \eta (\tilde{k}_{\oplus})^{XZ}],
\]

\[
c_{1} = \frac{\beta_{\oplus}}{2} \sin \chi \cos \chi \sin (\tilde{k}_{\ominus})^{YZ},
\]

\[
s_{2} = - \frac{\beta_{\oplus}}{4} (1 + \cos^{2} \chi) (\cos \eta + 1) (\tilde{k}_{\oplus})^{YZ},
\]

\[
c_{2} = - \frac{\beta_{\oplus}}{4} (1 + \cos^{2} \chi) (1 + \cos \eta) (\tilde{k}_{\ominus})^{XZ},
\]

\[
s_{2} = \frac{1}{2} (1 + \cos^{2} \chi) (\tilde{k}_{\ominus})^{XY},
\]

\[
c_{2} = \frac{1}{4} (1 + \cos^{2} \chi) [(\tilde{k}_{\ominus})^{XX} - (\tilde{k}_{\ominus})^{YY}],
\]

\[
s_{2} = \frac{\beta_{\oplus}}{4} (1 + \cos^{2} \chi)(1 - \cos \eta)(\tilde{k}_{\ominus})^{YZ},
\]

\[
c_{2} = \frac{\beta_{\oplus}}{4} (1 + \cos^{2} \chi)(1 - \cos \eta)(\tilde{k}_{\ominus})^{XZ}.
\]

It can be seen that the components of \(\tilde{k}_{\ominus}\) enter the experiment due to the movement of the laboratory with \(\beta_{\oplus}\). Each coefficient might include terms suppressed by either \(\beta_{\oplus}\), \(\beta_{L}\), or sin \(\Omega_{\oplus} \delta T\). These are only included if no term of larger order is present in the same coefficient. In effect, this removes all terms of order \(\beta_{L}\) and sin \(\Omega_{\oplus} \delta T\). The fit accuracy in the experiments does not allow us to resolve a suppressed term that occurs at the same frequency as an unsuppressed term.

From the nine components of \((\kappa_{F})_{\kappa_{0},\mu_{0}}\), that are not measured in astrophysical experiments, the parameter \(\kappa_{\eta}\) (17) does not lead to any time-dependent signals to first order in \(\beta_{\oplus}\) and \(\beta_{L}\) in any cavity experiment. On Earth, the parameter \((\tilde{k}_{\ominus})^{ZZ}\) is measurable only by using a turntable, because the rotation axis of the laboratory frame, i.e. Earth’s axis, coincides with the \(Z\) direction of the Sun-centered celestial equatorial reference frame adopted. The other seven independent parameter combinations can, however, be measured in our experiment.

### 2.2 Kinematic framework for SR tests

The Robertson–Mansouri–Sexl (RMS) framework [18] (see also [19] for a recent review) is a test theory of SR. According to this framework, SR follows from three experimental principles: the isotropy of the speed of light (MM test), the independence of the speed of light from the velocity of the laboratory (Kennedy–Thorpdike test), and time dilation. The last has been tested by laser spectroscopic measurement of the Doppler shift of relativistic atoms [20, 21], and will not be considered further here. MM tests currently offer the highest precision and are thus the most sensitive probe for possible violations of SR.

The framework offers a useful way of parameterizing violations of Lorentz invariance. A preferred frame \(\Sigma\), usu-
ally identified with the cosmic microwave background, is assumed, in which the speed of light $c_0$ is constant. The Lorentz transformations between $\Sigma$ and a frame $S$ moving with the velocity $v$ with respect to $\Sigma$ are replaced by generalized linear transformations. These depend solely on $v$ and three phenomenological parameters, which reduce to special values if SR holds. In the moving frame $S$, the speed of light can be expressed to lowest order in $v/c_0$ as

$$c_0^\prime = \frac{c_0}{\sqrt{1 - \frac{v^2}{c_0^2}}}.$$

(In the notation of [18] $A = -(\alpha - \beta + 1)$ and $B = -(\beta - \delta - 1/2)$. ) The dimensionless parameters $A$ and $B$ vanish if special relativity is valid; otherwise the speed of light may depend on $v$ and the angle $\theta$ between the direction of light propagation and $\mathbf{v}$. Kennedy–Thorne experiments test $A = 0$ (also called boost invariance), MM experiments test $B = 0$ (rotation invariance). $A = 1$ and $B = -1/2$ would be the predictions of the pre-relativistic ether theory.

2.2.1 Derivation of the signal for the Robertson–Mansouri–Sexty test theory.

This experiment. For this calculation, we may neglect Earth’s orbital velocity, as its inclusion would only lead to minor corrections to the hypothetical signal amplitudes as well as small signal components at additional frequencies, but would not enable us to measure additional parameters. The velocity vector $\mathbf{v}_{\text{ cmb}}$ of the motion of the Sun relative to the cosmic microwave background is given by the right ascension $\alpha = 168^\circ$ (or 11.2 h) and $\beta = -6^\circ$ declination at a speed of $v_{\text{ cmb}} = 369 \text{ km/s}$ [22]. In the Sun-centered frame as described in Sect. 2.1.1

$$v_{\text{ cmb}} = v_{\text{ cmb}} (-\cos \alpha \cos \beta, -\cos \alpha \sin \beta).$$

Our cavities are parallel to the $x$ and $y$ axes in the laboratory frame, respectively. Thus, the cavity orientations are given by the unit vectors $(e_x)_{\text{ lab}} = (1, 0, 0)$ and $(e_y)_{\text{ lab}} = (0, 1, 0)$. The rotations between the laboratory and the Sun-centered frames are given by the rotation matrix $R$ (19). The unit vectors describing the cavity orientations in the Sun-centered frame:

$$e_x = (\cos \chi \cos \omega_{\text{ lab}} T_{\text{ lab}}, \cos \chi \sin \omega_{\text{ lab}} T_{\text{ lab}}, -\sin \chi),$$

$$e_y = (-\sin \omega_{\text{ lab}} T_{\text{ lab}}, \cos \omega_{\text{ lab}} T_{\text{ lab}}, 0).$$

are thus obtained.

In our experiment, the difference of the frequencies

$$\frac{\Delta v_x}{v_0} - \frac{\Delta v_y}{v_0} = B \frac{v^2}{c_0^2} (\sin^2 \theta_x - \sin^2 \theta_y),$$

of the two cavities oriented south and east is measured, where $\theta_{x,y}$ are the angles of the cavity axes with respect to the direction of $v_{\text{ cmb}}$. $\theta_{1,2}$ are obtained within the Sun-centered frame by using

$$\sin^2 \theta_{x,y} = 1 - \frac{(v_{\text{ cmb}} e_x e_y)^2}{|v_{\text{ cmb}}|^2}. (29)$$

We find

$$\sin^2 \theta_x = 1 - \left[ -\cos \alpha \cos \beta \cos \chi \cos \omega_{\text{ lab}} T_{\text{ lab}} + \sin \beta \sin \chi - \cos \beta \cos \chi \sin \alpha \sin \omega_{\text{ lab}} T_{\text{ lab}} \right]^2.$$

$$\sin^2 \theta_y = 1 - \left[ -\cos \beta \cos \omega_{\text{ lab}} T_{\text{ lab}} \sin \alpha + \cos \beta \cos \alpha \sin \omega_{\text{ lab}} T_{\text{ lab}} \right]^2.$$

Using these expressions and simple trigonometric relations, we end up with

$$\frac{\Delta v}{v_0} = \frac{v^2}{v_0} (\gamma_1 \cos \omega_{\text{ lab}} T_{\text{ lab}} + \gamma_2 \cos 2\omega_{\text{ lab}} T_{\text{ lab}} + \sigma_1 \sin \omega_{\text{ lab}} T_{\text{ lab}} + \sigma_2 \sin 2\omega_{\text{ lab}} T_{\text{ lab}}),$$

where

$$\gamma_1 = 2 \cos \alpha \cos \beta \sin \beta \cos \chi,$$

$$\gamma_2 = -\frac{1}{2} \cos 2\alpha \cos^2 \beta (1 + \cos^2 \chi),$$

$$\sigma_1 = 2 \sin \alpha \cos \beta \sin \beta \cos \chi,$$

$$\sigma_2 = -\frac{1}{2} \sin 2 \alpha \cos \beta (1 + \cos^2 \chi).$$

The total signal amplitudes at $\omega_{\text{ lab}}$ and $2\omega_{\text{ lab}}$ are

$$\sqrt{\gamma_1^2 + \gamma_2^2} = 2 \cos \beta \sin \beta \cos \chi \sin \chi \approx 0.10,$$

$$\sqrt{\sigma_1^2 + \sigma_2^2} = \frac{1}{2} \cos^2 \beta (1 + \cos^2 \chi) \approx 0.77.$$

The experiment of Brillet and Hall. For comparison, we also calculate the signal components for the experiment of Brillet and Hall. Here, the frequency of a cavity rotating around the vertical axis has been compared to the frequency of a (non-rotating) methane frequency standard.

Assuming counterclockwise rotation with an angular frequency $\omega$, the cavity orientation in the laboratory frame is described by the unit vector

$$(e_{BH})_{\text{ lab}} = (\cos[\omega T_{\text{ lab}} + \phi_0], -\sin[\omega T_{\text{ lab}} + \phi_0], 0),$$

where the angle $\phi_0$ is between the orientation of the cavity at $T_{\text{ lab}} = 0$ and the laboratory $x$ axis. Rotating this into the Sun-centered frame and proceeding as above gives an expression for $\delta v/v$ containing oscillatory terms at many different frequencies that are summarized in Table 1.

Brillet and Hall reported the signal amplitudes that are the root of the sum of the squares of the sine and cosine components. These are given in Table 2.

2.3 Cavity orientation in the laboratory for optimum sensitivity

For technical reasons, both cavity axes should be horizontally oriented to minimize the gravitational influence on the cavities. Additionally, to provide maximum sensitivity, the two cavity axes should be normal to each other. The orientation of the cavities is chosen such that one cavity points north, the other east. On the one hand, this simplified fitting the experiment into our laboratory; on the other hand, it
3 Experimental aspects

Clearly, the challenges for performing parity tests using cavities are to

(i) minimize any mechanical effects that change the cavity length, and
(ii) minimize any errors that occur in the determination of the cavity frequency by means of the laser-frequency lock system.

In setting up our experiment, we have put substantial effort into satisfying these requirements.

3.1 Cryogenic resonators and experimental apparatus

Our COREs consist of a hollow 3-cm-long and 2.5-cm-diameter spacer and two mirrors fabricated from a single-crystal sapphire piece with the crystal $c$ axis parallel
to the cavity axis (see Fig. 4). After polishing and coating the mirror substrates with a multilayer high-reflectivity dielectric stack, they were optically contacted to the spacer, maintaining the original crystal orientation. The optical line widths of the two COREs used are 50 kHz and 100 kHz, respectively; the finesse is of order $10^3$.

The cryogenic operation of the sapphire resonators leads to a very low thermal expansion coefficient ($10^{-10}$/K at 4.2 K) and thus a low sensitivity to temperature changes. The creep of the cavities is not measurable at our current accuracy. Upper limits for the drift rates are $< 2$ kHz/6 months [12] and $< 0.1$ Hz/h [23]. These characteristics represent a significant advantage over usual room-temperature resonators made from non-crystalline ultra-low-expansion glass ceramics (ULE or zedur) that often exhibit drifts in the kHz/day range.

The COREs are operated inside a 4-K liquid-helium cryostat with optical access (see Fig. 5). The cryostat is equipped with a liquid-nitrogen shield. Liquid nitrogen is automat-
cally refilled about every 3 h, while liquid helium is manually refilled approx. every 2 days. The lasers employed are monolithic, diode-pumped Nd:YAG lasers (Lightwave Electronics, Inc. and Innolight GmbH) emitting at 1064 nm with a very narrow line width (< 10 kHz). The beams are coupled into the resonators passing through the cryostat windows.

3.2  

**Pound–Drever–Hall locking**

The requirement on the locking system is to provide the very best long-term stability. This differs from most other cavity frequency stabilization systems which are optimized to provide short-term stability (milliseconds to minutes).

For stabilizing a laser frequency $\omega_L$ to a resonance of a cavity at $\omega_{cav}$, we use a modified Pound–Drever–Hall (PDH) locking system together with a method for offset compensation (Sect. 3.4). For PDH locking a phase modulation (PM) with a frequency $\omega_m$ and a modulation index $\beta_m$ is applied to the laser beam. The beam is coupled to the cavity and the reflected signal is detected. The resonant and dispersive properties of the cavity near $\omega_{cav}$ convert the PM into amplitude modulation (AM) components at multiples of $\omega_m$. At zero detuning, the detected component of the AM vanishes; otherwise a non-zero AM can be detected. The detected signal is multiplied with a local oscillator (LO) signal at $\omega_m$ with a phase $\phi$ relative to the PM signal in a double-balanced mixer (DBM), and the output of the DBM is low-pass filtered to suppress the modulation frequency $\omega_m$. With the correct LO phase $\phi$, a PDH error signal with a zero crossing at $\omega_L = \omega_{cav}$ is generated. This signal is fed back to the laser-frequency actuator via a suitable servo, which controls (‘locks’) $\omega_L$ such that $\omega_L = \omega_{cav}$.

Our implementation of the PDH technique differs from the usual approach in that we use $3 \omega_m$ instead of $\omega_m$ as the LO frequency. This gives an error signal as shown in Fig. 6. The maximum signal amplitude is then obtained for a PM modulation index $\beta = 3.95$. A PM index of $\beta = 3.83$ (where the first sideband vanishes) is preferred for obtaining a signal without distortions from the first sideband, while losing only 1% of the signal amplitude. Compared to the usual $\omega_m$ technique, the $3 \omega_m$ method is relatively insensitive to residual AM produced by imperfections of the phase modulator. Theoretically, AM generates only first sidebands that do not contribute to the $3 \omega_m$ signal. Another advantage is that at the high modulation index used, most of the total laser power is contained in the sidebands. These do not enter the resonator if $\omega_m \gg B$. Consequently, the $3 \omega_m$ method generates an about two times better error signal S/N ratio at the same laser power circulating inside the cavity. Furthermore, the higher detection frequency $3 \omega_m$ helps to overcome the technical noise floor of the Nd : YAG laser.

It is important to keep the power of the light circulating inside the cavity as low as possible to minimize the change of the resonance frequency due to laser heating of the cavities, $\sim 10$ Hz/$\mu$W. At high laser powers, there seems to be a linear drift that is proportional to the laser power, but this was negligible for the low laser powers we employed. Using the $3 \omega_m$ technique and low-noise detection as described below, about 80 nW impinging on the COREs (not counting the laser power in the sidebands, that do not enter the CORE) was sufficient for locking with an error signal S/N ratio of $1.5 \times 10^4$/Hz. We reach a minimum instability of the locked laser frequency.

![FIGURE 6](image-url)  

**FIGURE 6** Measured Pound–Drever–Hall error signal generated by down conversion at $3 \omega_m$ LO frequency. The modulation index $\beta$ is 3.83, so that the first sideband vanishes. Otherwise, spikes would occur in the signal at $\omega_L = \omega_{cav} \pm 1 \omega_m$, between the central zero crossing and the zero crossing next to the center.

![FIGURE 7](image-url)  

**FIGURE 7**  

(a) Beat between two lasers locked using conventional PDH scheme. Shown is the lock error, the deviation of the lock point from the center of the cavity resonance, which was measured using the offset-compensation technique described in Sect. 3.4. The average lock error is about 900 Hz and varies by about 100 Hz peak to peak.  

(b) Same for two lasers locked using $3 \omega_m$ PDH lock. The average error is about 150 Hz, with variations of about 10 Hz peak to peak, mostly due to noise.
of $7 \times 10^{-16}$ for integration times between 150 and 450 s [10]. Figure 7 shows two time traces from beat measurements between lasers locked using 1 $\omega_m$ and 3 $\omega_m$ locking. The advantages of the 3 $\omega_m$ method are clearly visible. Thus this method has been used for all but a few measurements at the very beginning of the experiment.

Using even harmonics 2 $\omega_m$, 4 $\omega_m$, ..., no dispersive signal with a zero crossing at $\omega_m = \omega_{	ext{cv}}$ is generated. Instead, the 2 $\omega_m$ signal has a maximum at $\omega_m = \omega_{	ext{cv}}$. While the laser is locked, this can be used for a stray light insensitive measurement of the fraction of laser power that is coupled to the cavity. This signal has been used for optimizing the coupling of the laser beams to the COREs by the automatic beam-positioning system (see Sect. 3.3).

### 3.2.1 Phase modulation of the laser beam

The standard method for modulating the phase of the laser beam is to employ an electro-optic modulator (EOM). By using an EOM, however, it is difficult to reliably obtain residual amplitude modulation (RAM) levels below $10^{-3}$ on a long time scale. Thus we employ the alternative method of Nd:YAG laser crystal strain modulation. Here the excitation frequencies are chosen to coincide with mechanical resonances of the laser crystal near 500 kHz.

### 3.2.2 Detection and amplification of the light reflected from the COREs

The lock detectors are mounted rigidly to the CORE holder inside the cryostat to avoid a relative movement of the detectors and the COREs that could strongly distort the PDH error signal. We use Epitaxx 2000 InGaAs detectors with a large active detector area of 2 mm$^2$, which makes the detector position (that might be slightly changed during cooling) uncritical. The detector output current is brought out of the cryostat via about 2-m long, 50-$\Omega$ miniature coaxial cables.

The large detector area leads to a high capacitance of the detectors of about 500 pF. Application of reverse bias of 5 V reduces this to 170 pF. The cable capacity of 100 pF/m has to be added to this, totaling about 500 pF. At 3 $\omega_m \sim 1.5$ MHz, this has a reactance of only about $|X_C| \sim 300 \Omega$, making low current noise amplification of the detector signal extremely difficult. For reaching a current noise density $i_n$ on the order of pA/Hz$^{1/2}$, the amplifier must not only have such a low current noise, but also a voltage noise less than $i_n|X_C| \sim 300 \text{ pV/Hz}^{1/2}$. This corresponds to the noise generated by a 300-$\Omega$ resistor at a temperature of $\sim 5.4$ K.

As a first approach, we used a tank inductance to resonantly enhance $X_C$ by a factor $Q \sim 20$. The tank coil itself must have an extremely high $Q \sim 200$, so that the tank circuit’s $Q$ factor is limited by the detector loss and cable resistances that are at cryostat temperature. Otherwise, the series resistance of the inductance at room temperature would generate appreciable additional noise. With a first amplifier stage using a dual-gate MOSFET (type BF981), an overall equivalent detector current noise of about 2 pA/Hz$^{1/2}$ was reached. However, this approach requires cumbersome retuning for every modulation-frequency change and is unable to amplify the signal components at 2 $\omega_m$ (for measuring the in-coupling, see Sect. 3.3) and 3 $\omega_m$ (for locking) at the same time.

Thus we subsequently developed a broadband, paralleled MOSFET amplifier. The noise-voltage density at frequencies above the $1/f$ noise regime of a MOSFET can be roughly estimated by $u_n = (4k_B T r_n)^{1/2}$, where $T$ is the operating temperature near room temperature and $r_n \simeq 0.65/s$ [24], where $s$ is the transconductance of the FET. For low $u_n$, the transistors must therefore have high $s$, but at the same time low input capacitance $C_i$, in order not to reduce the input impedance further. MOSFET tetrodes BF1009 made for UHF receiver applications (by Infineon Technologies AG) were chosen. They have $C_i = 2.1$ pF and $s \simeq 30$ mS at 14 mA, so $u_n \simeq 600 \text{ pV/Hz}^{1/2}$ for a single transistor or $u_n \simeq 210 \text{ pV/Hz}^{1/2}$ for eight devices in parallel is expected. A further increase of the number of paralleled transistors makes it difficult to keep the amplifier stable because of the high transconductance and UHF capabilities of the devices.

While the detector reactance is mainly capacitive (and therefore noise-free), additional noise is generated by the resistance $R_C$ of the cable. At room temperature, $R_C \simeq 14 \Omega$, generating 400 pV/Hz$^{1/2}$. Fortunately, most of the cable is at the cryostat temperature and does not generate an appreciable noise contribution. The detector series resistance, also at 4 K, does contribute to the total noise as well. Overall, we reach a measured noise performance (with the cryostat cooled down) of about 3 pA/Hz$^{1/2}$, corresponding to an optical noise of 3.8 pW/Hz$^{1/2}$. Slight improvements by approximately equal factors were achieved by applying a photodetector backward bias of 4.5 V to decrease the detector capacitance and by using an impedance-matching transformer in front of the amplifier input. A 1 : 1.5 voltage ratio with the high-impedance side at the amplifier input was found to give lowest noise. Ultimately, we measured about 2.7 pW/Hz$^{1/2}$ equivalent optical noise power density, comparable to the resonant amplifier. This level corresponds to the shot noise of a $\sim 50$-μW beam. It allowed us to lock reliably at powers down to 80 nW impinging on the COREs.

### 3.2.3 Double-balanced-mixer operation

The selection and proper operation of the double-balanced mixer is crucial. On the one hand, it has to operate highly linearly to be able to suppress unwanted signal components. This requires a signal amplitude well below saturation. On the other hand, the signal amplitude should be large compared to the mixer offset voltages. Thus, a compromise is needed that often involves rather high drive levels. We, however, operate the mixer in a way that emphasizes linearity. This produced results superior to the ones obtained by a strong rf drive.

---

[1] For the Lightwave electronics laser, at a modulation frequency of 226 kHz, a PM index of 1 was obtained at $2 \times 10^{-5}$ RAM; the Innolight laser produced a PM index of 1 at RAM of $1.7 \times 10^{-4}$ (at 150 kHz). The AM components at 3 $\omega_m$ were below a level of $10^{-5}$ in both cases.

[2] These transfer a significant amount of heat into the cryostat; only two of these reduce the standing time by 20%; however, they have superior electrical performance compared to special cryostat coaxial cables.

[3] This reduces the sensitivity of the stabilized laser frequency to parameters such as laser-power variations, beam alignment, polarization, or electromagnetic interference. These influences produce error-signal amplitude and phase changes, and also parasitic signals at other than the LO frequency. A non-linear DBM converts these to a DC signal that adds an offset to the error signal.
3.3 Beam-alignment stabilization

An automatic beam-alignment stabilization is used to compensate for the movements of the COREs located inside the cryostats that are caused by refills and evaporation of coolants. These movements change the lock point, in part due to coupling to higher modes of the cavities and inhomogeneity of the lock detectors’ active area, and possibly additional reasons.

For alignment stabilization, the laser beams pass through glass plates mounted under an angle of 45° relative to the beams, thus causing a parallel displacement of the beams. The angle can be controlled by ±6° using galvanometer drives, corresponding to a ±50-μm adjustment range of the beam displacement. For each beam, one glass plate controls the x and one the y displacement. A displacement error signal is generated by dithering the tilt angles at frequencies in the range of 300–1000 Hz. The laser power coupled to the COREs is measured and analyzed by lock-in amplifiers referenced to the tilt-angle modulation signal. This produces an incoupling error signal that is zero when the incoupling is optimum. Separate signals can be obtained for each galvanometer by using different modulation frequencies. The galvanometer tilt angle is then controlled by slow I servos.

As a stray light insensitive measure of the coupling efficiency, we use the 2ωm PDH error signal produced by the lock detectors in reflection. The amplitude of this signal is proportional to the laser power coupled into the cavity, while stray light that hits the detector without having entered the cavity before does not contribute.

3.4 Offset compensation

Using the PDH system, lock errors originate (i) from the generation and modulation of the oscillations (e.g. residual AM caused by the phase modulator), (ii) from the transmission of the oscillations to the reference (like parasitic resonances in the signal path), and (iii) from the generation of the error signal \( U_e \) (like temperature dependence of electronic circuits). For such reasons, a signal \( U_e + U_0 \) is generated instead of \( U_e \). The lock point, where \( U_e + U_0 = 0 \), is thus shifted to \( \omega_{res} + \varepsilon_0 \).

Since these influences can never be fully removed, a method is desirable to measure and compensate for these influences. We developed and successfully applied such a method (OCAMS = offset compensation by amplitude-modulated sidebands), which is the subject of a separate publication [25]. During several months of the measurement another previously developed method was implemented, which achieved a compensation of offsets on the error signal in a different way. Here an additional phase modulation with a constant amplitude was done at 10 MHz for the first (respectively 25 MHz for the second) laser using EOMs. Every 5 s

\[ \delta U / U_{\text{max}} (10–50\%) \]

\[ \text{Type} \quad \text{Designation} \quad \delta U / U_{\text{max}} (10–50\%) \]

\[ \text{SAY-1 (a)} \quad 23 \text{ dBm mixer} \quad 133 \text{ ppm} \]

\[ \text{SAY-1 (b)} \quad 23 \text{ dBm mixer} \quad 166 \text{ ppm} \]

\[ \text{ZAD1-1} \quad 7 \text{ dBm mixer} \quad 700 \text{ ppm} \]

\[ \text{ZAD-8 (a)} \quad 7 \text{ dBm mixer} \quad < 25 \text{ ppm} \]

\[ \text{ZAD-8 (b)} \quad 7 \text{ dBm mixer} \quad 50 \text{ ppm} \]

\[ \text{ZRPD-1 (a)} \quad \text{Phase detector} \quad 3000 \text{ ppm}^a \]

\[ \text{ZRPD-1 (b)} \quad \text{Phase detector} \quad 20000 \text{ ppm}^a \]

\[ \text{Type} \quad \text{Designation} \quad \Delta U / U_{\text{max}} \]

\[ \text{SAY-1 (a)} \quad 23 \text{ dBm mixer} \quad 133 \text{ ppm} \]

\[ \text{SAY-1 (b)} \quad 23 \text{ dBm mixer} \quad 166 \text{ ppm} \]

\[ \text{ZAD1-1} \quad 7 \text{ dBm mixer} \quad 700 \text{ ppm} \]

\[ \text{ZAD-8 (a)} \quad 7 \text{ dBm mixer} \quad < 25 \text{ ppm} \]

\[ \text{ZAD-8 (b)} \quad 7 \text{ dBm mixer} \quad 50 \text{ ppm} \]

\[ \text{ZRPD-1 (a)} \quad \text{Phase detector} \quad 3000 \text{ ppm}^a \]

\[ \text{ZRPD-1 (b)} \quad \text{Phase detector} \quad 20000 \text{ ppm}^a \]

\[ ^a \text{This might be the result of improper handling prior to this measurement: exceeding the maximum ratings of the mixer can cause unbalance between the diodes inside the DBM, although it does not necessarily lead to complete failure.} \]

\[ ^b \text{With the very low light levels we use, these are sometimes surprisingly strong, especially due to switching power supplies and horizontal deflection coils in instrumentation equipment of modern make (i.e. unshielded with plastic housing).} \]
alternately the sideband of one of the lasers was automatically locked to the cavity instead of the carrier for 1 s. After that the carrier was automatically relocked again.

As the error signals produced by carrier and sidebands are of different amplitude, the offset on these signals, which is very nearly frequency independent, leads to different lock-point shifts when locking the carrier and the sidebands. From the measured beat frequencies during each locking interval, values for the lock-point shifts of both lasers \( \epsilon_{\text{OCC}, x, y} \) are calculated by a computer and correction signals can be added to the error signals via a D/A converter.

The correction signals were generated as the measured lock-point shifts \( \epsilon_{\text{OCC}, x, y} \) times factors \( A_x \) and \( A_y \), plus the sum \( \sum U_{\text{corr}, x, y} \) of all past correction voltages. This is to approximate an integral servo, which means that a constant offset is suppressed below any desired value after sufficient integration time. The constants were adjusted such that the time constant for suppressing an offset to about 1/2 of its original value was some 100 s.

The improvements in insensitivity of the beat frequency to external influences, which were achieved by applying active offset compensation, are summarized in Table 5.

### Table 5

<table>
<thead>
<tr>
<th>Laser Type</th>
<th>( \delta )</th>
<th>( \delta_{\text{I}} ) [Hz]</th>
<th>( \delta_{\text{I}}^{OC} ) [Hz]</th>
</tr>
</thead>
<tbody>
<tr>
<td>LO phase laser 1</td>
<td>10°</td>
<td>1200</td>
<td>&lt; 10</td>
</tr>
<tr>
<td>LO phase laser 2</td>
<td>10°</td>
<td>80</td>
<td>&lt; 10</td>
</tr>
<tr>
<td>( \beta_0 ) laser 1</td>
<td>+1%</td>
<td>50</td>
<td>—</td>
</tr>
<tr>
<td>( \beta_0 ) laser 2</td>
<td>+20%</td>
<td>—</td>
<td>—20</td>
</tr>
<tr>
<td>DBM temp.</td>
<td>30°C</td>
<td>30...50</td>
<td>&lt; 10</td>
</tr>
<tr>
<td>Laser power laser 1</td>
<td>4%</td>
<td>50</td>
<td>—</td>
</tr>
<tr>
<td>Laser power laser 2</td>
<td>30%</td>
<td>—</td>
<td>25</td>
</tr>
</tbody>
</table>

4 Data analysis

Except for a 10-day break around New Year 2002, during which polarizers were installed in the cryostat, the COREs were operated continuously at 4.2 K over more than one year. Usable data (discounting data sets shorter than 12 h and data taken during adjustment or liquid-helium refills) started on June 19, 2001 and was acquired over 390 days until July 13, 2002.

4.1 Cleaning and fitting the data

In order to produce reliable and reproducible results an automated procedure for analyzing the data was developed. This was complicated by the fact that data of different quality had been obtained during the 390 days of measurement, e.g. because new techniques were tested. The crucial point here was to find objective criteria to distinguish perturbed data sets from data sets considered to be usable for an analysis, and to remove a few single outliers from a single data set.

For analyzing the data, it was first averaged into one-minute bins to reduce the amount of data points. Figure 8 shows a part of the raw data including several usable measurement periods that each show frequency fluctuations of some tens of Hz or less, separated by off-lock periods, e.g. due to helium refills and adjustments. Sometimes, especially in the first days after cooling down the cryostat, relaxation of mechanical strain built up during cooling causes permanent frequency shifts between the data sets. The off-lock periods were eliminated by hand and the data sets showing no such permanent shifts over at least 12 h were selected. This was the only manual action taken in the analysis. To remove large spikes (up to several MHz) still included in some of the remaining data (e.g. due to accidental interruption of the laser beam that enters the beat detector), all data points more than 100 kHz away from the average of a data set were removed. Thus, 146 pre-cleaned data sets of 12 h to 109 h in length were obtained.

To obtain limits on Lorentz violation in the frameworks provided by the SME or the RMS test theory, the pre-cleaned data is analyzed for a hypothetical sinusoidal isotropy violation signal at the frequencies suggested by the test theories.

For analysis at frequencies \( 2\nu_0, 2\nu_0 - \Omega_0, \) and \( 2\nu_0 + \Omega_0 \) only data sets > 12 h in length are considered. Similarly, for \( \nu_0, \nu_0 - \Omega_0, \) and \( \nu_0 + \Omega_0 \) only data sets > 24 h are included. The pre-cleaned data sets are divided into subsets of 12 h (24h). This removes a fraction of the data as remaining < 12 h (< 24 h) are discarded, but makes the fit results independent of offsets in the data. 199 non-overlapping, independent subsets of 12 h and 43 subsets of 24 h were used in total. In analyzing a subset we proceed as follows (Fig. 9): the average and standard deviation of the data subset are calculated. Points that deviate from the average by more than five standard deviations are discarded. Since at this stage the data usually contains a drift of 10–100 Hz/h and the standard deviation is correspondingly large, this is a very weak criterion. It removes large spikes that would lead to erroneous results in the final fitting procedure (see inset in Fig. 9). To remove possible remaining outliers, the subset is fitted with a constant
offset and a linear drift, and the average square deviation $\bar{\chi}^2$ of the data from the fit is calculated. Data points that deviate from the fit by more than $3\sqrt{\bar{\chi}^2}$ are discarded. This cleaning removes only a minute amount of data (< 1%).

The cleaned data subsets are least-squares fitted with the amplitude and phase of a sinusoidal signal at frequencies given by RMS or SME with offset and linear drift as free parameters. As a measure for the quality of a data set, the average $\bar{\chi}^2$ of the squared residuals for each fit was calculated. As a minimum requirement for the fit quality, we took $\sqrt{\bar{\chi}^2} < 20$ Hz. This criterion was violated for 25 subsets of 12 h and one subset of 24 h. In these cases, the first 1–3 h of the pre-cleaned data set (that likely contained perturbations from a preceding helium refill) were discarded, and the cleaning and fitting procedure was repeated with the subsequent 12 h. This allowed us to re-introduce eight of the 25 perturbed 12-h subsets into the analysis.

The average and standard error calculated from the distribution of the individual fit results were taken as the final result. Coherent (vector) averaging was used, i.e. the fitted amplitude and phase of the individual data sets were projected onto the sine and cosine components of the hypothetical signal prior to averaging.

The above cleaning and fitting procedure has been carried through completely automated by a computer program. To check the reliability of the method and the program, test data sets were constructed by superimposing an artificial signal of known amplitude (between 10 Hz and 50 Hz) and phase on the complete 390 days of actual data, with all interruptions, outliers, etc. The test data sets were then run through the above procedure, and the results obtained were compared to the known amplitude of the artificial signal. It was found that the fit results obtained were equal to the artificial signal amplitude within an error that was consistent with the error bar of the results (see Fig. 10).

4.2 Final result in the RMS framework

For the analysis within the RMS formalism, the hypothetical signal consists of components at $\omega_B$ and $2\omega_B$ (35). The fit results for these frequencies in principle allow us to deduce two independent limits on the RMS anisotropy parameter $B$; however, the limit from the $\omega_B$ fit result is weaker. For the $2\omega_B$ component, we obtain a signal of 1.03 ± 0.53 Hz, or $\Delta c/c = (3.7 \pm 1.9) \times 10^{-15}$. As the data quality is not uniform, (Fig. 11), taking a weighted average is more appropriate. We divide the data into the groups A–E with approximately uniform data quality within each. The average and standard error of each interval are then calculated (Table 6). These results are then combined for the final result weighted according to their standard error. Thus, we obtain a signal amplitude of 0.73 ± 0.48 Hz, or $\Delta c/c = (2.6 \pm 1.7) \times 10^{-15}$.

\[ \text{FIGURE 9} \quad \text{Removal of outliers and fit of violation signal in a 12-h data subset. Large spikes (see inset) are omitted by dropping all data points beyond} \ 5\sqrt{\chi^2} \text{ in a first step. Then a linear drift and offset are fitted to the data and all points more than} \ 3\sqrt{\chi^2} \text{ away from the fit (dotted lines) are considered outliers and are dropped. The remaining data points are least-squares fitted with a sinusoidal signal corresponding to RMS or SME with offset and linear drift as free parameters.} \]

\[ \text{FIGURE 10 Left: Histogram of SME-fit results at cos} \ 2\omega_B t \text{ from the original data. Right: Histogram of fit results at cos} \ 2\omega_B t \text{ from the original data plus a sinusoidal test data set of 10 Hz \cdot cos} \ 2\omega_B t \]

\[ \text{FIGURE 11 Distribution of RMS-fit results over time for signals at cos} \ 2\omega_B t \text{ and distribution of fit residuals. The data is grouped into five sections of different quality. The histograms for each single group are shown below, the mean values and standard errors of which are given in Table 6.} \]
additional (but weaker) limits on the elements of the symmetric matrix, which enters the experiment suppressed by $\beta_\phi$. Thus, all elements of $\tilde{k}_{\phi}$ and all but one element of $\tilde{k}_{\psi}$ are obtained. Our results can be compared to the ones by Lipa et al. [9]. Their values are generally of order $10^{-13}$ for $\tilde{k}_{\psi}$ and of order $10^{-9}$ for $\tilde{k}_{\phi}$; thus, our measurement has an accuracy about two orders of magnitude higher. Furthermore, while [9] gives linear combinations of the components of $\tilde{k}_{\phi}$, our experiment allows individual determination. This is because the $>1$-yr span of our data allows us to separate results for all six signal frequencies.

5 Summary and outlook

In conclusion, we have performed a modern Michelson–Morley experiment that compared the frequencies of two crossed cryogenic optical resonators subject to Earth’s rotation over more than one year. The limit we obtained on the isotropy-violation parameter within the Robertson–Mansouri–Sexl framework is about three times lower than that from the experiment of Brillet and Hall [8]. Furthermore, we obtained limits on seven parameters from the photonic sector of the standard model extension [6], at accuracies down to $10^{-15}$, which is about two orders of magnitude lower than the only previous result [9].

For a future setup of the experiment active rotation on a turntable could improve the accuracy significantly. The low drift of COREs compared to ULE cavities allows a relatively slow rotation rate, which is desirable for minimizing the systematic errors connected to active rotation. At a rate of $\sim 0.2/\text{min}$ the optimum $\sim 7 \times 10^{-16}$ frequency stability of the COREs at integration times of $\tau = 100$ s could be utilized, which is more than 10 times better than on the 12-h time scale used so far. Accumulating $\sim 500$ measurements per day (two per turn), one should thus be able to reach the $10^{-17}$ level of accuracy. Further improvements include fiber coupling and COREs of higher finesse. New state of the art COREs should be able to offer a 10-fold decrease in line width, which should directly lead to a corresponding improvement in lock stability. Altogether a 100–1000-fold improvement in accuracy should be within reach in the near future.

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